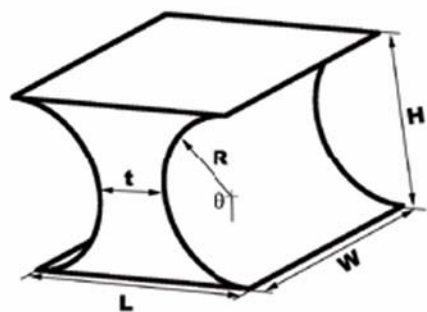


Appendix C

STIFFNESS APPROXIMATIONS FOR FEA OF COUPLING SIMULATION

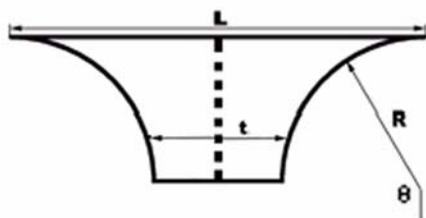
+ **Mathcad Sheet to Find Parameters of CAD Geometry for Equivalent Coupling Stiffness in FEA**

To find compliance or stiffness of substitute geometry:

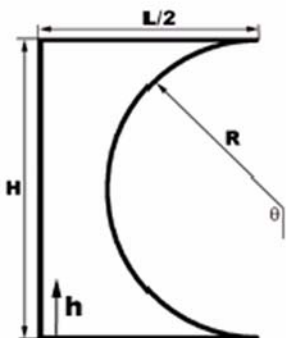


$$k_z = \frac{E \cdot A}{L} = \frac{E \cdot t \cdot W}{H}$$

W and L are constant to size of coupling
H, t, R, and θ are used to get approximated stiffness in z-direction



$$t = L - 2 \cdot R \cdot \sin(\theta)$$



$$R = \frac{H}{2}$$

$$h = \frac{H}{2} \cdot (1 - \cos(\theta))$$

$$h = R \cdot (1 - \cos(\theta))$$

Which gives stiffness as a function of θ :

$$k_z(\theta) = \frac{E \cdot (L - 2 \cdot R \cdot \sin(\theta)) \cdot W}{R \cdot (1 - \cos(\theta))}$$

For overall thickness of geometry, integrate over 180 degrees:

$$k_z = \int_0^\pi \frac{E \cdot (L - 2 \cdot R \cdot \sin(\theta)) \cdot W}{R \cdot (1 - \cos(\theta))} d\theta$$

Since denominator in integral will cause a singularity, invert to find the compliance of the geometry.

$$C_z = \int_0^\pi \frac{R \cdot (1 - \cos(\theta))}{E \cdot (L - 2R \cdot \sin(\theta)) \cdot w} d\theta$$

Invert resulting compliance to find stiffness. Repeat until a radius R or height H is found that gives an equivalent stiffness.

Example Calculation:

Input Stiffness from Kinematic Coupling Analysis:

$$k_{KC} := 9.95178 \times 10^7 \frac{\text{N}}{\text{m}}$$

$$k_{KC_per_coupling} := \frac{k_{KC}}{3} \quad k_{KC_per_coupling} = 3.317 \times 10^7 \frac{\text{N}}{\text{m}}$$

Input Basic Dimensions and Properties of Coupling Material:

$$E := 29.9938 \times 10^6 \text{ psi}$$

$$L := 35 \text{ mm}$$

$$W := 35 \text{ mm}$$

Define equation for coupling stiffness in terms of the height:

$$C_z(h) := \int_0^\pi \frac{\frac{h}{2} \cdot (1 - \cos(\theta))}{E \cdot (L - h \cdot \sin(\theta)) \cdot W} d\theta \quad k_z(h) := \frac{1}{C_z(h)}$$

Iterate to find optimal value of h:

$$h_{opt} := \begin{cases} h_{test} \leftarrow L \\ \text{while } k_z(h_{test}) \leq k_{KC_per_coupling} \\ \quad h_{test} \leftarrow h_{test} - .00001 \cdot \text{mm} \\ h_{test} \end{cases}$$

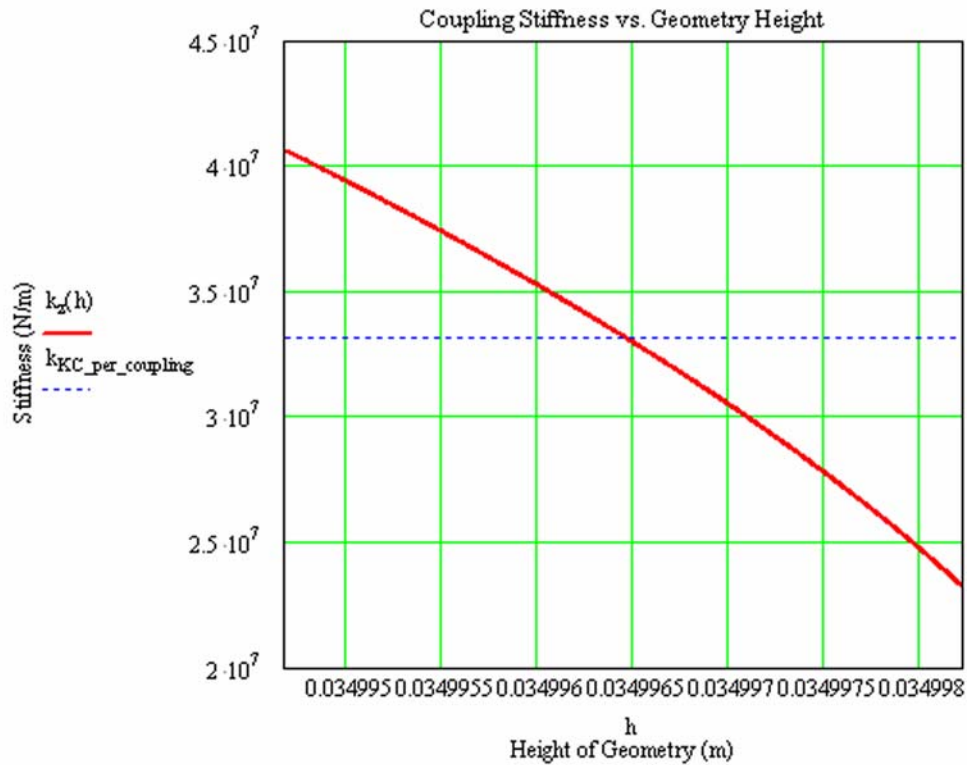
$$h_{opt} = 34.99645 \text{ mm}$$

$$k_z(h_{opt}) = 3.31815 \times 10^7 \frac{\text{N}}{\text{m}}$$

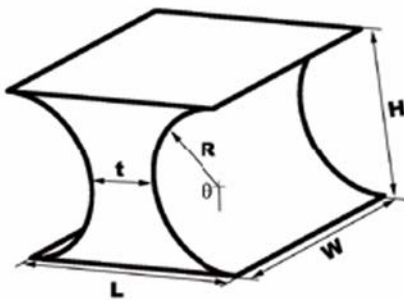
Error of iteration step:

$$\text{error} := \frac{k_z(h_{\text{opt}}) - k_{\text{KC_per_coupling}}}{k_{\text{KC_per_coupling}}} \quad \text{error} = 0.027\%$$

And a plot of coupling stiffness versus the height of the geometry:



So, final geometric parameters are as follows for a stiffness of $k_z(h_{\text{opt}}) = 3.318 \times 10^7 \frac{\text{N}}{\text{m}}$



$$W = 35 \text{ mm}$$

$$L = 35 \text{ mm}$$

$$H := h_{\text{opt}}$$

$$H = 34.996 \text{ mm}$$

$$R := \frac{H}{2}$$

$$R = 17.498 \text{ mm}$$

$$t := L - 2R$$

$$t = 3.55 \times 10^{-3} \text{ mm}$$

Equivalent Coupling Stiffness in FEA using Young's Modulus Approximation

$$L := 21\text{mm}$$

$$K_{kc} := 9.95178 \times 10^7 \frac{\text{N}}{\text{m}}$$

$$A := 35\text{mm} \cdot 35\text{mm}$$

$$E := \frac{L \cdot K_{kc}}{3 \cdot A}$$

$$E = 5.687 \times 10^8 \text{ Pa}$$

